

(Z)-3-Ferrocenyl-2-phenylacrylonitrile

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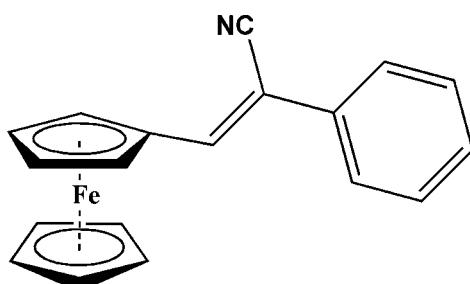
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Key indicators: single-crystal X-ray study; $T = 293\text{ K}$; mean $\sigma(\text{C}-\text{C}) = 0.005\text{ \AA}$; disorder in main residue; R factor = 0.053; wR factor = 0.127; data-to-parameter ratio = 17.1.

In the structure of the title compound, $[\text{Fe}(\text{C}_5\text{H}_5)(\text{C}_{14}\text{H}_{10}\text{N})]$, the unsubstituted cyclopentadiene (Cp) ring is disordered over two positions, with site-occupancy factors 0.76 (2) and 0.24 (2). The dihedral angles between the substituted Cp ring and the major and the minor components of the disordered ring are 0.9 (5) and 6(2) $^\circ$, respectively. The plane of the acrylonitrile unit makes dihedral angles of 6.1 (18) and 6.5 (4) $^\circ$ with the substituted Cp ring and the phenyl ring planes, respectively.

Related literature

For background to the chemistry of ferrocene, see: Long (1995); Roberto *et al.* (2000); Togni & Hayashi (1995). For the structures of ferrocene derivatives, see: Base *et al.* (2002); Hess *et al.* (1999). For bond distances in the acrylonitrile unit, see: Allen *et al.* (1987).



Experimental

Crystal data

$[\text{Fe}(\text{C}_5\text{H}_5)(\text{C}_{14}\text{H}_{10}\text{N})]$
 $M_r = 313.17$
Monoclinic, $P2_1/c$
 $a = 6.8255$ (14) \AA
 $b = 11.795$ (2) \AA
 $c = 19.939$ (4) \AA
 $\beta = 106.786$ (16) $^\circ$

$V = 1536.8$ (5) \AA^3
 $Z = 4$
Mo $K\alpha$ radiation
 $\mu = 0.97\text{ mm}^{-1}$
 $T = 293$ (2) K
 $0.18 \times 0.06 \times 0.05\text{ mm}$

Data collection

Rigaku, SCXmini diffractometer
Absorption correction: multi-scan (*CrystalClear*; Rigaku, 2005)
 $T_{\min} = 0.892$, $T_{\max} = 1.00$
(expected range = 0.850–0.953)

15093 measured reflections
3523 independent reflections
2520 reflections with $I > 2\sigma(I)$
 $R_{\text{int}} = 0.050$

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.052$
 $wR(F^2) = 0.126$
 $S = 1.07$
3523 reflections
206 parameters

30 restraints
H-atom parameters constrained
 $\Delta\rho_{\max} = 0.22\text{ e \AA}^{-3}$
 $\Delta\rho_{\min} = -0.40\text{ e \AA}^{-3}$

Data collection: *CrystalClear* (Rigaku, 2005); cell refinement: *CrystalClear*; data reduction: *CrystalClear*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *SHELXTL* (Sheldrick, 2008); software used to prepare material for publication: *SHELXL97*.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: SJ2497).

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supplementary materials

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(Z)-3-Ferrocenyl-2-phenylacrylonitrile

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Comment

The chemistry of ferrocene has received much attention because of its applications in many fields, such as in catalysis, organic or organometallic synthesis and materials (Togni, *et al.* (1995)). The use of ferrocene and its derivatives as non-linear optical(NLO) materials has also been reported (Long, 1995; Roberto *et al.*, 2000). As part of our on going studies of the chemistry of ferrocene, we present here the structure of the title compound, (Z)-2-Phenyl-3-(ferrocenyl)acrylonitrile (I).

In I, the unsubstituted cyclopentadienyl (Cp) ring is disordered over two positions, the site occupancy factors are 0.76 (2) and 0.24 (2). The major disorder component is nearly parallel to the substituted Cp ring with a dihedral angle of 0.9 (5) $^{\circ}$, and the rings are in an eclipsed configuration with the torsion angle C1-Cg1-Cg2-C10, -5.918 (3) $^{\circ}$. The minor component of the disordered Cp ring is tilted slightly, making a dihedral of 6(2) $^{\circ}$ with C1…C5, and the rings are staggered, C1-Cg1-Cg2'-C9' 44.692 (4) $^{\circ}$ (Cg(1) denotes the centroid of the C1…C5 Cp ring, Cg(2) and Cg(2)' denote the centroids of the C6…C10 and C6'…C10' rings respectively). Fe-C distances to the substituted Cp ring vary from 2.030 (3) to 2.039 (3) \AA , and are in the normal ranges (Hess *et al.*, 1999; Base *et al.*, 2002). Those to the unsubstituted Cp ring cover a wider range from 1.92 (3) to 2.084 (7) \AA . The iron-ring centroid distances are Fe–Cg(1), 1.6378 (16) \AA , Fe–Cg(2) 1.674 (3) \AA and Fe–Cg(2)' 1.594 (13) \AA . Within the acrylonitrile unit, bond angles and the C11=C12 double bond distance, 1.345 (3) \AA and C19≡N1 distances, 1.142 (4) \AA , are normal (Allen *et al.* (1987). The plane of acrylonitrile unit makes dihedral angles of 6.13 (1.81) $^{\circ}$ and 6.52 (0.39) $^{\circ}$ with the C1…C5 ring and the C13…C18 phenyl ring plane, respectively.

Experimental

To a mixture of ferrocenecarboxaldehyde and 2-phenyletonitrile in CH₂Cl₂ was added pyrrolidine and the mixture was heated to reflux temperature for 3 h. The reaction was cooled to room temperature and solvent removed. The crude product was purified by column chromatography on silica gel using ethyl acetate-petroleum ether (v:v, 1:3) as eluent to collect the main yellow band. Red crystals suitable for X-ray analysis were obtained by slow evaporation of a saturated solution of ethyl acetate-petroleum ether (v:v,1:3). BAND YELLOW, CRYSTALS RED. IS THIS CORRECT??

Refinement

All H-atoms were positioned geometrically and refined using a riding model with d(C-H) = 0.93 \AA , U_{iso}=1.2U_{eq} (C). The unsubstituted Cp ring is disordered over two positions with site occupancy factors 0.76 (2) and 0.24 (2) respectively; corresponding C atoms were restrained to have the same anisotropic displacement parameters.

supplementary materials

Figures

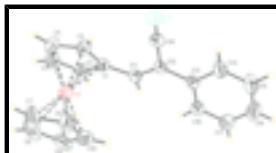


Fig. 1. The structure of I showing the atom numbering scheme with displacement ellipsoids drawn at the 30% probability level. For clarity only atoms of the major disorder component of the unsubstituted cyclopentadiene ring are included.

(Z)-3-Ferrocenyl-2-phenylacrylonitrile

Crystal data

| | |
|---|---|
| [Fe(C ₅ H ₅)(C ₁₄ H ₁₀ N)] | $F_{000} = 648$ |
| $M_r = 313.17$ | $D_x = 1.354 \text{ Mg m}^{-3}$ |
| Monoclinic, $P2_1/c$ | Mo $K\alpha$ radiation |
| Hall symbol: -P 2ybc | $\lambda = 0.71073 \text{ \AA}$ |
| $a = 6.8255 (14) \text{ \AA}$ | Cell parameters from 2947 reflections |
| $b = 11.795 (2) \text{ \AA}$ | $\theta = 3.1\text{--}27.5^\circ$ |
| $c = 19.939 (4) \text{ \AA}$ | $\mu = 0.97 \text{ mm}^{-1}$ |
| $\beta = 106.786 (16)^\circ$ | $T = 293 (2) \text{ K}$ |
| $V = 1536.8 (5) \text{ \AA}^3$ | Block, red |
| $Z = 4$ | $0.18 \times 0.06 \times 0.05 \text{ mm}$ |

Data collection

| | |
|--|--|
| Rigaku, SCXmini diffractometer | 3523 independent reflections |
| Radiation source: fine-focus sealed tube | 2520 reflections with $I > 2\sigma(I)$ |
| Monochromator: graphite | $R_{\text{int}} = 0.050$ |
| Detector resolution: 13.6612 pixels mm ⁻¹ | $\theta_{\text{max}} = 27.5^\circ$ |
| $T = 293(2) \text{ K}$ | $\theta_{\text{min}} = 3.1^\circ$ |
| ω scans | $h = -8 \rightarrow 8$ |
| Absorption correction: Multi-scan (CrystalClear; Rigaku, 2005) | $k = -15 \rightarrow 15$ |
| $T_{\text{min}} = 0.892$, $T_{\text{max}} = 1.00$ | $l = -25 \rightarrow 25$ |
| 15093 measured reflections | |

Refinement

| | |
|---------------------------------|--|
| Refinement on F^2 | Secondary atom site location: difference Fourier map |
| Least-squares matrix: full | Hydrogen site location: inferred from neighbouring sites |
| $R[F^2 > 2\sigma(F^2)] = 0.053$ | H-atom parameters constrained |
| $wR(F^2) = 0.126$ | $w = 1/[\sigma^2(F_o^2) + (0.0496P)^2 + 0.4337P]$ |
| $S = 1.07$ | where $P = (F_o^2 + 2F_c^2)/3$ |
| | $(\Delta/\sigma)_{\text{max}} < 0.001$ |

3523 reflections $\Delta\rho_{\max} = 0.22 \text{ e \AA}^{-3}$
 206 parameters $\Delta\rho_{\min} = -0.40 \text{ e \AA}^{-3}$
 30 restraints Extinction correction: none
 Primary atom site location: structure-invariant direct methods

Special details

Geometry. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted R -factor wR and goodness of fit S are based on F^2 , conventional R -factors R are based on F , with F set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating R -factors(gt) etc. and is not relevant to the choice of reflections for refinement. R -factors based on F^2 are statistically about twice as large as those based on F , and R -factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (\AA^2)

| | x | y | z | $U_{\text{iso}}^*/U_{\text{eq}}$ | Occ. (<1) |
|------|-------------|-------------|--------------|----------------------------------|-----------|
| Fe1 | 0.27058 (7) | 0.42653 (4) | 0.29905 (2) | 0.06096 (17) | |
| N1 | -0.4172 (4) | 0.4888 (3) | 0.12481 (18) | 0.0911 (10) | |
| C1 | 0.1205 (4) | 0.3903 (2) | 0.19717 (14) | 0.0537 (6) | |
| C2 | 0.2972 (5) | 0.3198 (3) | 0.22231 (17) | 0.0701 (8) | |
| H2A | 0.4135 | 0.3160 | 0.2029 | 0.084* | |
| C3 | 0.2759 (7) | 0.2573 (3) | 0.2800 (2) | 0.0887 (11) | |
| H3A | 0.3752 | 0.2028 | 0.3077 | 0.106* | |
| C4 | 0.0914 (7) | 0.2867 (3) | 0.2915 (2) | 0.0922 (12) | |
| H4A | 0.0394 | 0.2566 | 0.3289 | 0.111* | |
| C5 | -0.0077 (5) | 0.3694 (3) | 0.24149 (17) | 0.0714 (8) | |
| H5A | -0.1400 | 0.4052 | 0.2377 | 0.086* | |
| C6 | 0.2256 (9) | 0.5813 (5) | 0.3412 (3) | 0.0813 (15) | 0.764 (8) |
| H6A | 0.0944 | 0.6208 | 0.3326 | 0.098* | 0.764 (8) |
| C7 | 0.3062 (13) | 0.4980 (6) | 0.3956 (3) | 0.105 (2) | 0.764 (8) |
| H7A | 0.2460 | 0.4729 | 0.4322 | 0.125* | 0.764 (8) |
| C8 | 0.4978 (13) | 0.4657 (7) | 0.3864 (4) | 0.113 (2) | 0.764 (8) |
| H8A | 0.5923 | 0.4107 | 0.4158 | 0.136* | 0.764 (8) |
| C9 | 0.5340 (9) | 0.5257 (7) | 0.3301 (4) | 0.0948 (17) | 0.764 (8) |
| H9A | 0.6548 | 0.5189 | 0.3133 | 0.114* | 0.764 (8) |
| C10 | 0.3661 (11) | 0.5945 (6) | 0.3021 (4) | 0.0794 (17) | 0.764 (8) |
| H10A | 0.3473 | 0.6441 | 0.2613 | 0.095* | 0.764 (8) |
| C6' | 0.270 (3) | 0.5375 (19) | 0.3729 (13) | 0.0813 (15) | 0.236 (8) |
| H6'A | 0.1502 | 0.5559 | 0.3885 | 0.098* | 0.236 (8) |
| C7' | 0.421 (5) | 0.452 (2) | 0.4048 (12) | 0.105 (2) | 0.236 (8) |
| H7'A | 0.4250 | 0.4022 | 0.4445 | 0.125* | 0.236 (8) |
| C8' | 0.562 (4) | 0.457 (3) | 0.3629 (14) | 0.113 (2) | 0.236 (8) |
| H8'A | 0.6793 | 0.4061 | 0.3681 | 0.136* | 0.236 (8) |

supplementary materials

| | | | | | |
|------|-------------|------------|---------------|-------------|-----------|
| C9' | 0.488 (4) | 0.534 (3) | 0.3082 (11) | 0.0948 (17) | 0.236 (8) |
| H9'A | 0.5544 | 0.5509 | 0.2718 | 0.114* | 0.236 (8) |
| C10' | 0.315 (4) | 0.588 (3) | 0.3162 (16) | 0.0794 (17) | 0.236 (8) |
| H10B | 0.2395 | 0.6496 | 0.2872 | 0.095* | 0.236 (8) |
| C11 | 0.1004 (4) | 0.4723 (2) | 0.14174 (13) | 0.0480 (6) | |
| H11A | 0.2197 | 0.4875 | 0.1297 | 0.058* | |
| C12 | -0.0664 (4) | 0.5297 (2) | 0.10511 (13) | 0.0452 (6) | |
| C13 | -0.0704 (4) | 0.6196 (2) | 0.05293 (13) | 0.0483 (6) | |
| C14 | -0.2528 (5) | 0.6672 (3) | 0.01394 (16) | 0.0699 (8) | |
| H14A | -0.3752 | 0.6405 | 0.0197 | 0.084* | |
| C15 | -0.2574 (6) | 0.7535 (3) | -0.03341 (19) | 0.0869 (11) | |
| H15A | -0.3820 | 0.7844 | -0.0589 | 0.104* | |
| C16 | -0.0805 (7) | 0.7933 (3) | -0.04285 (19) | 0.0854 (11) | |
| H16A | -0.0838 | 0.8524 | -0.0740 | 0.103* | |
| C17 | 0.1036 (6) | 0.7462 (3) | -0.00626 (19) | 0.0788 (10) | |
| H17A | 0.2244 | 0.7721 | -0.0136 | 0.095* | |
| C18 | 0.1093 (5) | 0.6603 (3) | 0.04146 (16) | 0.0636 (7) | |
| H18A | 0.2345 | 0.6293 | 0.0663 | 0.076* | |
| C19 | -0.2607 (4) | 0.5059 (2) | 0.11687 (15) | 0.0588 (7) | |

Atomic displacement parameters (\AA^2)

| | U^{11} | U^{22} | U^{33} | U^{12} | U^{13} | U^{23} |
|------|-------------|-------------|-------------|--------------|-------------|--------------|
| Fe1 | 0.0733 (3) | 0.0567 (3) | 0.0496 (2) | -0.0014 (2) | 0.0125 (2) | 0.00379 (19) |
| N1 | 0.0504 (16) | 0.114 (3) | 0.110 (3) | -0.0086 (16) | 0.0258 (16) | 0.017 (2) |
| C1 | 0.0581 (16) | 0.0510 (14) | 0.0512 (15) | -0.0058 (13) | 0.0147 (13) | -0.0008 (12) |
| C2 | 0.083 (2) | 0.0592 (18) | 0.0641 (18) | 0.0146 (16) | 0.0151 (16) | 0.0034 (15) |
| C3 | 0.118 (3) | 0.0534 (19) | 0.082 (2) | 0.005 (2) | 0.009 (2) | 0.0107 (17) |
| C4 | 0.115 (3) | 0.081 (2) | 0.077 (2) | -0.029 (2) | 0.023 (2) | 0.022 (2) |
| C5 | 0.0686 (19) | 0.082 (2) | 0.0657 (19) | -0.0166 (17) | 0.0221 (16) | 0.0088 (17) |
| C6 | 0.121 (4) | 0.063 (3) | 0.060 (3) | 0.006 (3) | 0.026 (3) | -0.005 (2) |
| C7 | 0.183 (7) | 0.075 (4) | 0.046 (3) | 0.018 (4) | 0.020 (4) | 0.001 (2) |
| C8 | 0.133 (6) | 0.107 (4) | 0.068 (6) | 0.021 (4) | -0.022 (3) | -0.021 (4) |
| C9 | 0.070 (4) | 0.107 (4) | 0.085 (5) | -0.015 (3) | -0.013 (3) | -0.019 (4) |
| C10 | 0.089 (5) | 0.066 (2) | 0.082 (4) | -0.019 (3) | 0.023 (3) | -0.008 (2) |
| C6' | 0.121 (4) | 0.063 (3) | 0.060 (3) | 0.006 (3) | 0.026 (3) | -0.005 (2) |
| C7' | 0.183 (7) | 0.075 (4) | 0.046 (3) | 0.018 (4) | 0.020 (4) | 0.001 (2) |
| C8' | 0.133 (6) | 0.107 (4) | 0.068 (6) | 0.021 (4) | -0.022 (3) | -0.021 (4) |
| C9' | 0.070 (4) | 0.107 (4) | 0.085 (5) | -0.015 (3) | -0.013 (3) | -0.019 (4) |
| C10' | 0.089 (5) | 0.066 (2) | 0.082 (4) | -0.019 (3) | 0.023 (3) | -0.008 (2) |
| C11 | 0.0455 (14) | 0.0553 (14) | 0.0461 (14) | 0.0003 (12) | 0.0177 (11) | -0.0021 (12) |
| C12 | 0.0406 (13) | 0.0525 (14) | 0.0433 (13) | -0.0017 (11) | 0.0135 (11) | -0.0073 (11) |
| C13 | 0.0522 (14) | 0.0519 (14) | 0.0394 (13) | 0.0001 (12) | 0.0108 (11) | -0.0072 (11) |
| C14 | 0.0583 (17) | 0.088 (2) | 0.0609 (18) | 0.0090 (16) | 0.0133 (15) | 0.0151 (16) |
| C15 | 0.082 (2) | 0.102 (3) | 0.069 (2) | 0.023 (2) | 0.0105 (19) | 0.025 (2) |
| C16 | 0.114 (3) | 0.076 (2) | 0.065 (2) | 0.004 (2) | 0.025 (2) | 0.0182 (18) |
| C17 | 0.082 (2) | 0.078 (2) | 0.077 (2) | -0.0134 (19) | 0.0245 (19) | 0.0116 (18) |
| C18 | 0.0584 (17) | 0.0674 (19) | 0.0616 (18) | -0.0044 (15) | 0.0119 (14) | 0.0060 (15) |

| | | | | | | |
|-----|-------------|-------------|-------------|--------------|-------------|-------------|
| C19 | 0.0492 (16) | 0.0637 (17) | 0.0605 (17) | −0.0033 (14) | 0.0112 (13) | 0.0009 (14) |
|-----|-------------|-------------|-------------|--------------|-------------|-------------|

Geometric parameters (\AA , $^\circ$)

| | | | |
|--------------|------------|------------|------------|
| Fe1—C9' | 1.92 (3) | C8—H8A | 0.9800 |
| Fe1—C10' | 1.94 (3) | C9—C10 | 1.383 (7) |
| Fe1—C6' | 1.970 (19) | C9—H9A | 0.9800 |
| Fe1—C8 | 2.023 (7) | C10—H10A | 0.9800 |
| Fe1—C5 | 2.029 (3) | C6'—C10' | 1.388 (17) |
| Fe1—C2 | 2.030 (3) | C6'—C7' | 1.451 (18) |
| Fe1—C4 | 2.032 (4) | C6'—H6'A | 0.9800 |
| Fe1—C3 | 2.034 (4) | C7'—C8' | 1.445 (19) |
| Fe1—C1 | 2.039 (3) | C7'—H7'A | 0.9800 |
| Fe1—C7 | 2.051 (5) | C8'—C9' | 1.396 (18) |
| Fe1—C8' | 2.06 (3) | C8'—H8'A | 0.9800 |
| Fe1—C6 | 2.069 (5) | C9'—C10' | 1.393 (17) |
| N1—C19 | 1.142 (4) | C9'—H9'A | 0.9800 |
| C1—C2 | 1.431 (4) | C10'—H10B | 0.9800 |
| C1—C5 | 1.433 (4) | C11—C12 | 1.345 (3) |
| C1—C11 | 1.445 (4) | C11—H11A | 0.9300 |
| C2—C3 | 1.409 (5) | C12—C19 | 1.439 (4) |
| C2—H2A | 0.9800 | C12—C13 | 1.480 (4) |
| C3—C4 | 1.387 (5) | C13—C14 | 1.382 (4) |
| C3—H3A | 0.9800 | C13—C18 | 1.396 (4) |
| C4—C5 | 1.419 (5) | C14—C15 | 1.383 (5) |
| C4—H4A | 0.9800 | C14—H14A | 0.9300 |
| C5—H5A | 0.9800 | C15—C16 | 1.359 (5) |
| C6—C10 | 1.408 (8) | C15—H15A | 0.9300 |
| C6—C7 | 1.449 (7) | C16—C17 | 1.375 (5) |
| C6—H6A | 0.9800 | C16—H16A | 0.9300 |
| C7—C8 | 1.424 (10) | C17—C18 | 1.382 (4) |
| C7—H7A | 0.9800 | C17—H17A | 0.9300 |
| C8—C9 | 1.408 (10) | C18—H18A | 0.9300 |
| C9'—Fe1—C10' | 42.3 (7) | C4—C5—Fe1 | 69.7 (2) |
| C9'—Fe1—C6' | 70.2 (8) | C1—C5—Fe1 | 69.73 (17) |
| C10'—Fe1—C6' | 41.5 (6) | C4—C5—H5A | 126.3 |
| C9'—Fe1—C8 | 52.3 (7) | C1—C5—H5A | 126.3 |
| C10'—Fe1—C8 | 65.3 (9) | Fe1—C5—H5A | 126.3 |
| C6'—Fe1—C8 | 51.1 (7) | C10—C6—C7 | 108.5 (5) |
| C9'—Fe1—C5 | 147.7 (7) | C10—C6—Fe1 | 70.6 (4) |
| C10'—Fe1—C5 | 119.9 (8) | C7—C6—Fe1 | 68.8 (3) |
| C6'—Fe1—C5 | 116.1 (6) | C10—C6—H6A | 125.7 |
| C8—Fe1—C5 | 157.2 (3) | C7—C6—H6A | 125.7 |
| C9'—Fe1—C2 | 104.1 (8) | Fe1—C6—H6A | 125.7 |
| C10'—Fe1—C2 | 134.2 (8) | C8—C7—C6 | 104.4 (6) |
| C6'—Fe1—C2 | 174.3 (6) | C8—C7—Fe1 | 68.5 (3) |
| C8—Fe1—C2 | 125.3 (3) | C6—C7—Fe1 | 70.1 (3) |
| C5—Fe1—C2 | 68.93 (14) | C8—C7—H7A | 127.8 |
| C9'—Fe1—C4 | 166.9 (9) | C6—C7—H7A | 127.8 |

supplementary materials

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| C10'—Fe1—C4 | 150.3 (8) | Fe1—C7—H7A | 127.8 |
| C6'—Fe1—C4 | 117.6 (7) | C9—C8—C7 | 110.3 (7) |
| C8—Fe1—C4 | 123.0 (3) | C9—C8—Fe1 | 72.3 (4) |
| C5—Fe1—C4 | 40.89 (14) | C7—C8—Fe1 | 70.6 (4) |
| C2—Fe1—C4 | 67.89 (17) | C9—C8—H8A | 124.8 |
| C9'—Fe1—C3 | 127.5 (9) | C7—C8—H8A | 124.8 |
| C10'—Fe1—C3 | 169.8 (8) | Fe1—C8—H8A | 124.8 |
| C6'—Fe1—C3 | 142.7 (8) | C10—C9—C8 | 107.5 (6) |
| C8—Fe1—C3 | 109.5 (3) | C10—C9—Fe1 | 70.5 (4) |
| C5—Fe1—C3 | 68.47 (16) | C8—C9—Fe1 | 67.7 (4) |
| C2—Fe1—C3 | 40.58 (14) | C10—C9—H9A | 126.2 |
| C4—Fe1—C3 | 39.89 (15) | C8—C9—H9A | 126.2 |
| C9'—Fe1—C1 | 112.6 (6) | Fe1—C9—H9A | 126.2 |
| C10'—Fe1—C1 | 112.9 (8) | C9—C10—C6 | 109.2 (5) |
| C6'—Fe1—C1 | 140.8 (8) | C9—C10—Fe1 | 70.7 (4) |
| C8—Fe1—C1 | 161.0 (3) | C6—C10—Fe1 | 69.7 (3) |
| C5—Fe1—C1 | 41.24 (12) | C9—C10—H10A | 125.4 |
| C2—Fe1—C1 | 41.19 (12) | C6—C10—H10A | 125.4 |
| C4—Fe1—C1 | 68.75 (13) | Fe1—C10—H10A | 125.4 |
| C3—Fe1—C1 | 68.87 (13) | C10'—C6'—C7' | 110.9 (15) |
| C9'—Fe1—C7 | 76.2 (7) | C10'—C6'—Fe1 | 68.1 (16) |
| C10'—Fe1—C7 | 57.4 (8) | C7'—C6'—Fe1 | 73.2 (14) |
| C6'—Fe1—C7 | 18.4 (6) | C10'—C6'—H6'A | 124.6 |
| C8—Fe1—C7 | 40.9 (3) | C7'—C6'—H6'A | 124.6 |
| C5—Fe1—C7 | 120.3 (3) | Fe1—C6'—H6'A | 124.6 |
| C2—Fe1—C7 | 161.9 (3) | C8'—C7'—C6' | 103.2 (14) |
| C4—Fe1—C7 | 108.0 (2) | C8'—C7'—Fe1 | 68.6 (16) |
| C3—Fe1—C7 | 125.1 (2) | C6'—C7'—Fe1 | 64.9 (13) |
| C1—Fe1—C7 | 155.6 (3) | C8'—C7'—H7'A | 128.4 |
| C9'—Fe1—C8' | 40.9 (6) | C6'—C7'—H7'A | 128.4 |
| C10'—Fe1—C8' | 69.4 (9) | Fe1—C7'—H7'A | 128.4 |
| C6'—Fe1—C8' | 68.5 (8) | C9'—C8'—C7' | 109.1 (16) |
| C8—Fe1—C8' | 20.8 (6) | C9'—C8'—Fe1 | 64.2 (15) |
| C5—Fe1—C8' | 170.4 (8) | C7'—C8'—Fe1 | 70.5 (16) |
| C2—Fe1—C8' | 107.0 (7) | C9'—C8'—H8'A | 125.2 |
| C4—Fe1—C8' | 129.7 (8) | C7'—C8'—H8'A | 125.2 |
| C3—Fe1—C8' | 102.6 (8) | Fe1—C8'—H8'A | 125.2 |
| C1—Fe1—C8' | 140.3 (7) | C10'—C9'—C8' | 109.5 (16) |
| C7—Fe1—C8' | 61.1 (7) | C10'—C9'—Fe1 | 69.7 (17) |
| C9'—Fe1—C6 | 65.3 (9) | C8'—C9'—Fe1 | 74.9 (16) |
| C10'—Fe1—C6 | 25.6 (7) | C10'—C9'—H9'A | 125.2 |
| C6'—Fe1—C6 | 22.8 (6) | C8'—C9'—H9'A | 125.2 |
| C8—Fe1—C6 | 67.4 (3) | Fe1—C9'—H9'A | 125.2 |
| C5—Fe1—C6 | 107.3 (2) | C6'—C10'—C9' | 107.1 (15) |
| C2—Fe1—C6 | 155.4 (2) | C6'—C10'—Fe1 | 70.3 (14) |
| C4—Fe1—C6 | 126.1 (2) | C9'—C10'—Fe1 | 68.0 (17) |
| C3—Fe1—C6 | 162.6 (2) | C6'—C10'—H10B | 126.5 |
| C1—Fe1—C6 | 119.9 (2) | C9'—C10'—H10B | 126.5 |
| C7—Fe1—C6 | 41.2 (2) | Fe1—C10'—H10B | 126.5 |

| | | | |
|------------|-------------|--------------|-----------|
| C8'—Fe1—C6 | 80.0 (7) | C12—C11—C1 | 129.1 (2) |
| C2—C1—C5 | 106.7 (3) | C12—C11—H11A | 115.4 |
| C2—C1—C11 | 122.8 (3) | C1—C11—H11A | 115.4 |
| C5—C1—C11 | 130.3 (3) | C11—C12—C19 | 119.3 (2) |
| C2—C1—Fe1 | 69.07 (17) | C11—C12—C13 | 125.7 (2) |
| C5—C1—Fe1 | 69.03 (17) | C19—C12—C13 | 115.0 (2) |
| C11—C1—Fe1 | 122.09 (19) | C14—C13—C18 | 117.4 (3) |
| C3—C2—C1 | 108.4 (3) | C14—C13—C12 | 121.1 (2) |
| C3—C2—Fe1 | 69.9 (2) | C18—C13—C12 | 121.5 (2) |
| C1—C2—Fe1 | 69.74 (17) | C13—C14—C15 | 121.5 (3) |
| C3—C2—H2A | 125.8 | C13—C14—H14A | 119.3 |
| C1—C2—H2A | 125.8 | C15—C14—H14A | 119.3 |
| Fe1—C2—H2A | 125.8 | C16—C15—C14 | 120.2 (3) |
| C4—C3—C2 | 108.4 (3) | C16—C15—H15A | 119.9 |
| C4—C3—Fe1 | 70.0 (2) | C14—C15—H15A | 119.9 |
| C2—C3—Fe1 | 69.55 (19) | C15—C16—C17 | 120.0 (3) |
| C4—C3—H3A | 125.8 | C15—C16—H16A | 120.0 |
| C2—C3—H3A | 125.8 | C17—C16—H16A | 120.0 |
| Fe1—C3—H3A | 125.8 | C16—C17—C18 | 120.1 (3) |
| C3—C4—C5 | 109.1 (3) | C16—C17—H17A | 120.0 |
| C3—C4—Fe1 | 70.1 (2) | C18—C17—H17A | 120.0 |
| C5—C4—Fe1 | 69.45 (19) | C17—C18—C13 | 120.9 (3) |
| C3—C4—H4A | 125.4 | C17—C18—H18A | 119.6 |
| C5—C4—H4A | 125.4 | C13—C18—H18A | 119.6 |
| Fe1—C4—H4A | 125.4 | N1—C19—C12 | 178.3 (3) |
| C4—C5—C1 | 107.4 (3) | | |

supplementary materials

Fig. 1

